

DESIGN OF ACTIVE FLOW CONTROL AT THE WING/PYLON/ENGINE JUNCTION

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2ND GENERATION
ACTIVE WING

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Outline

- Motivation
- Baseline geometry and flow
- Pulsed blowing actuation
- Synthetic jet actuation
- Full aircraft scale evaluation
- Summary and conclusions



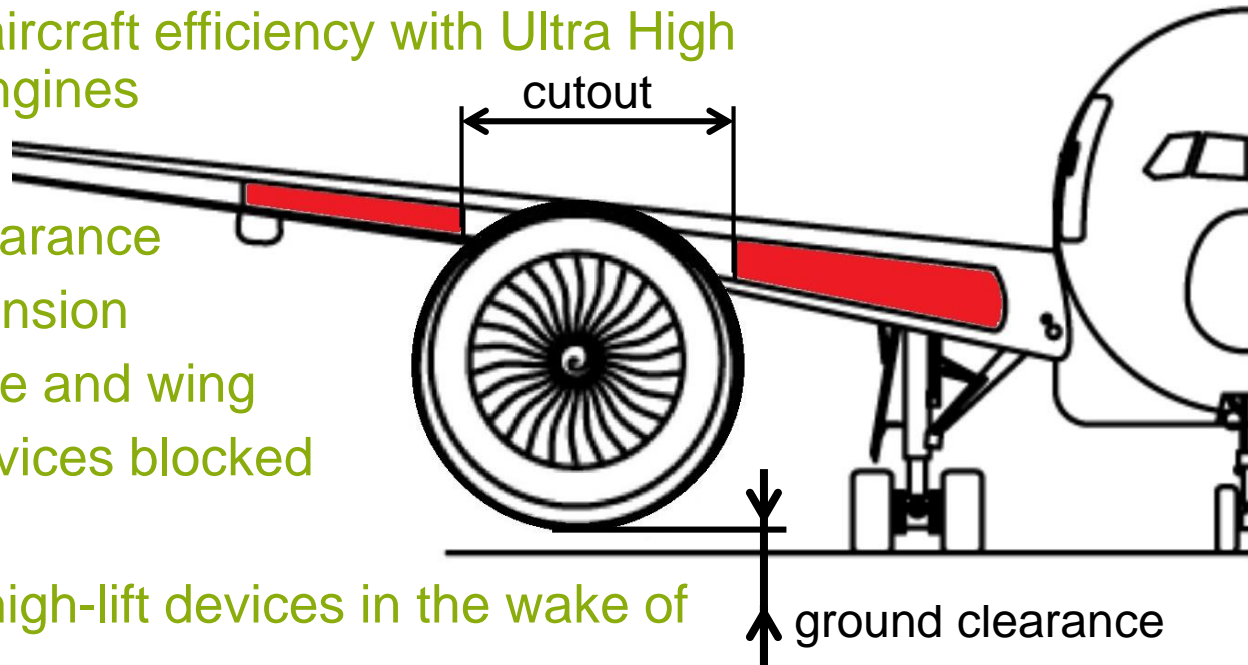


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MOTIVATION

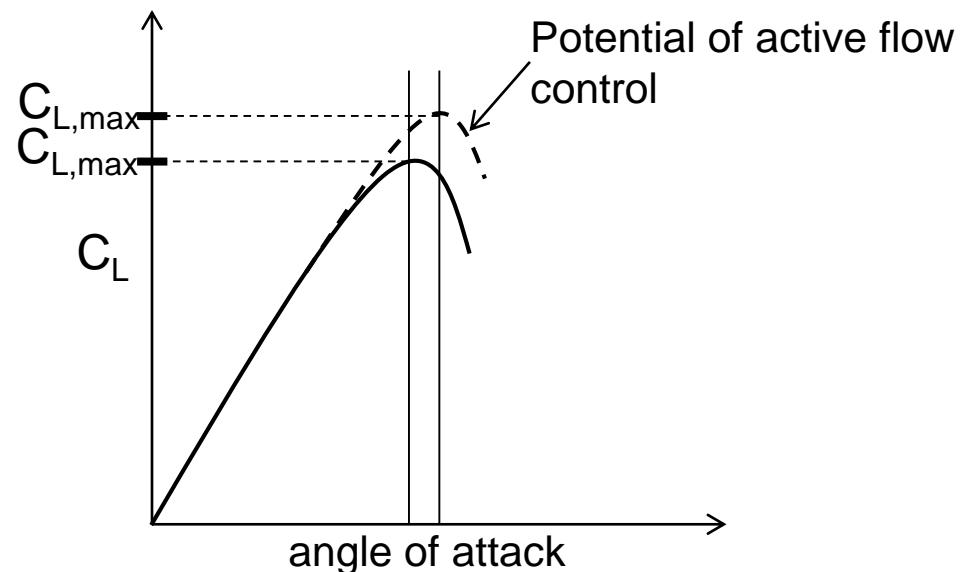
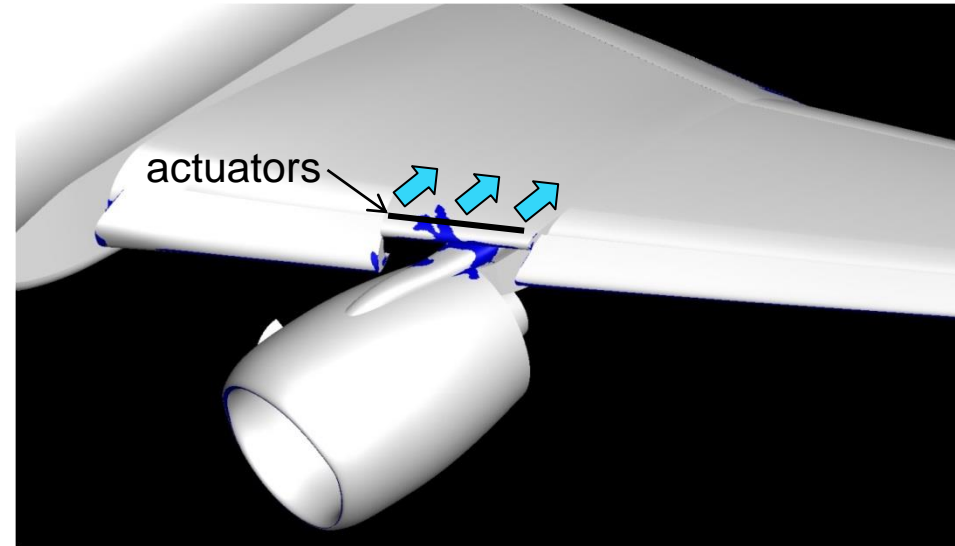
Motivation

- Modern transport aircraft configuration with engines mounted under the wing
- Further increase of the aircraft efficiency with Ultra High Bypass Ratio (UHBR) engines
- Larger nacelle diameter
- Problem with ground clearance
- Heavy landing gear extension
- Closer coupling of engine and wing
- leading edge high-lift devices blocked by the engine nacelle
- Cutout of leading edge high-lift devices in the wake of the nacelle



Motivation

- Separation in the wake of the nacelle triggers the total wing stall which limits the $C_{L,max}$
- $C_{L,max}$ is a sizing parameter of the high-lift system
- Heavy high-lift system counteracts benefit by UHBR
- Local separation can be suppressed by active flow control
- $C_{L,max}$ increases which allows a downsizing of the high-lift system
- Increase of overall aircraft efficiency by local application of active flow control



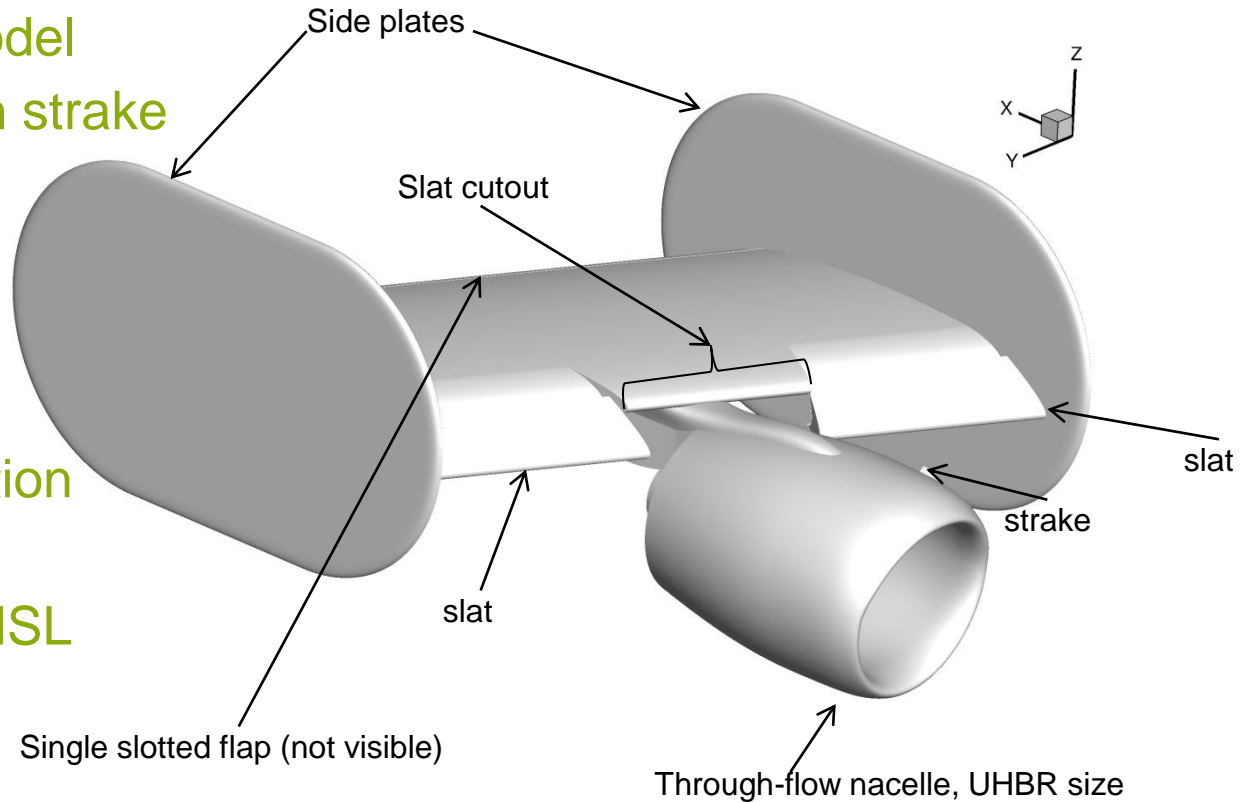
The logo for AFLoNext, featuring the text "AFLoNext" in a sans-serif font. The "o" is stylized with a green and blue swoosh underneath it.

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BASELINE GEOMETRY AND FLOW

Wind Tunnel Geometry

- Full scale 2.5D model
- UHBR nacelle with strake
- Wing span: 5.8m
- Chord: 3.29m
- DLR F15-profile
- Sweep angle: 28°
- Landing configuration
- $M=0.2$
- ISA condition on MSL
- $Re=15 \times 10^6$

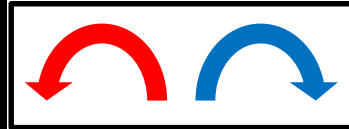
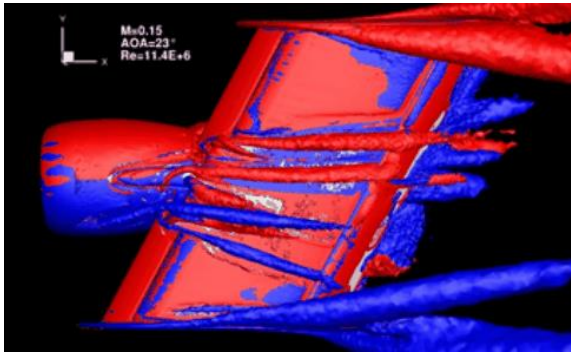


Realistic vs. Wind tunnel configuration

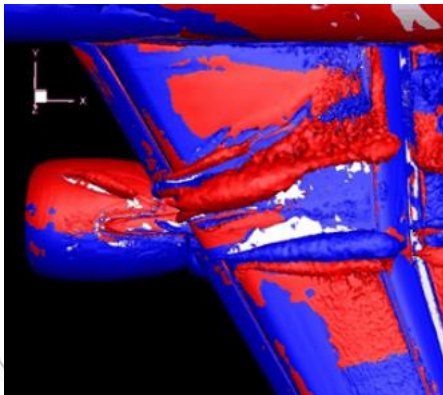
- Vortex structure depends on the level of simplification
- Separated areas similar – from pylon axis inboard
 - Mirrored!

Vortices

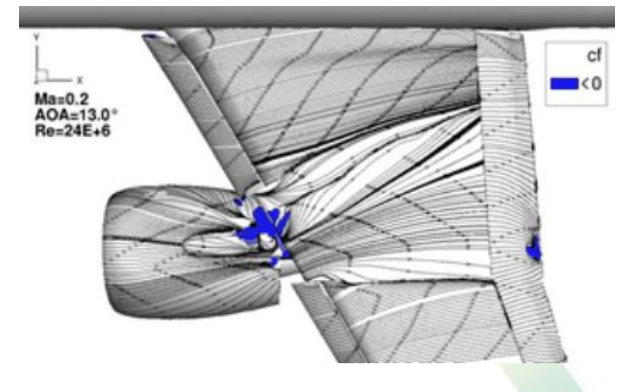
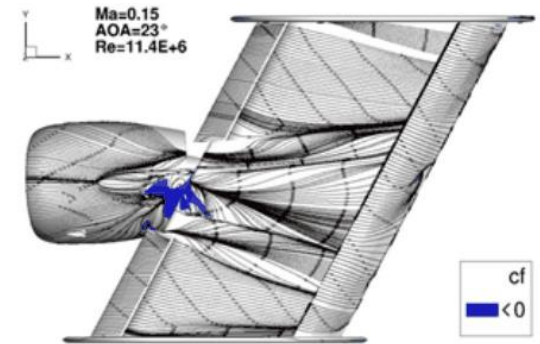
Baseline Configuration



Realistic Configuration

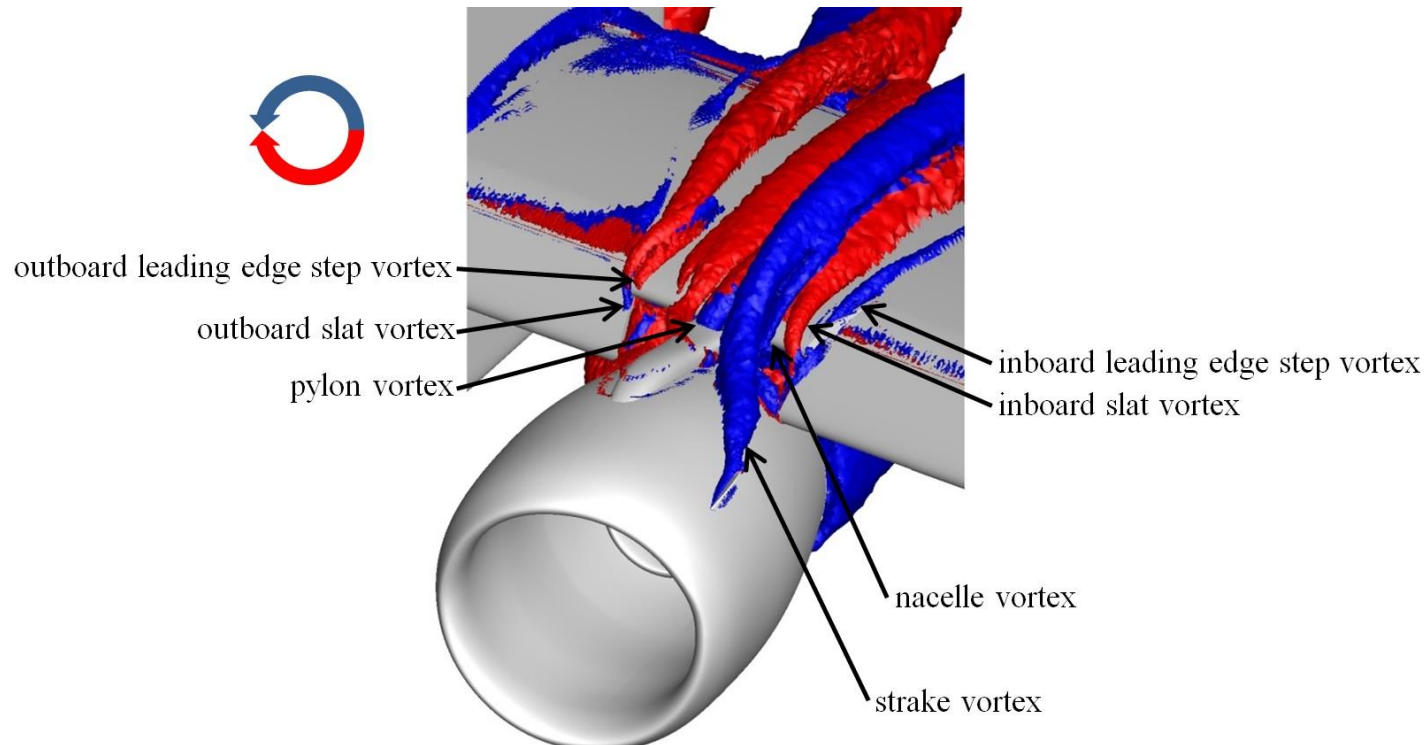


Separation areas



Results: Baseline Flow

- Vortices at pre-stall conditions
- made visible with the λ_2 -criteria
- Sense of rotation made visible with ω_x



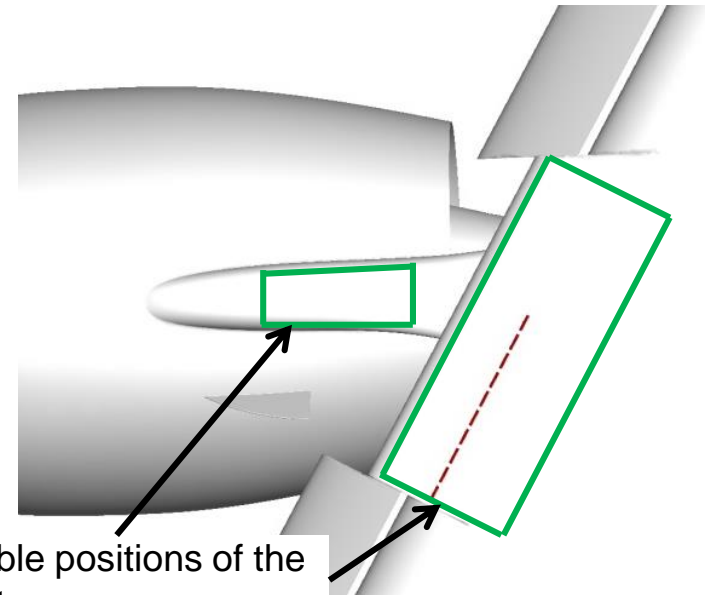
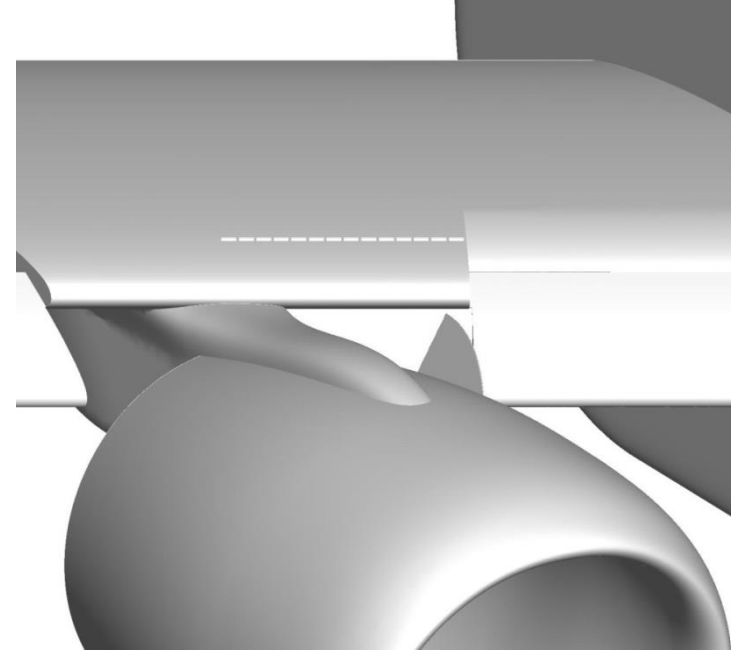


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PULSED BLOWING

PJA - design problem

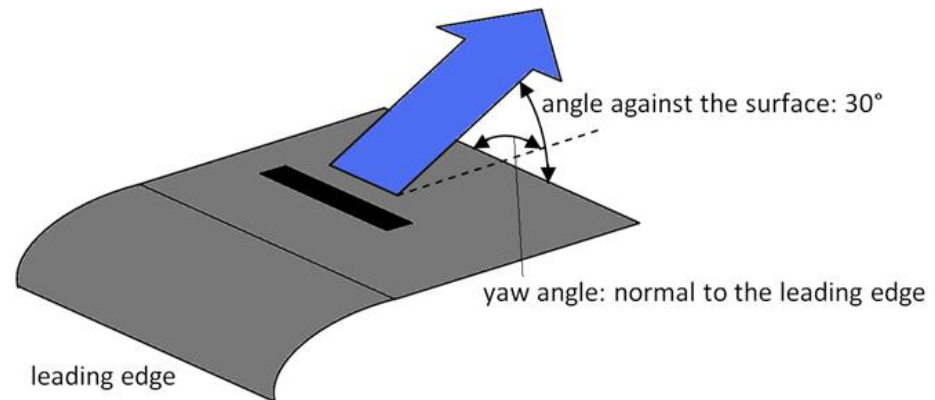
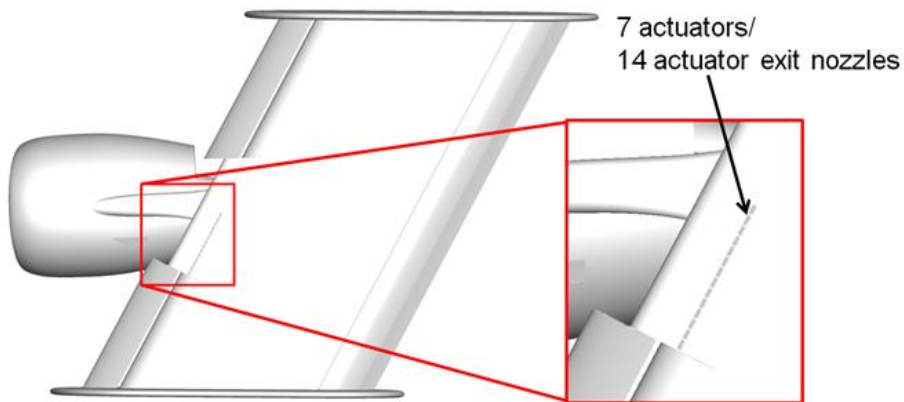
- Pulsed jet actuators
 - Air injected
- Design parameter of the actuators
 - Slit size
 - Number of actuators
 - Blow velocity
 - Pulse frequency
 - Blowing direction
- Position of the actuators
- Position of the strake
- Very large parameter space



Possible positions of the actuators

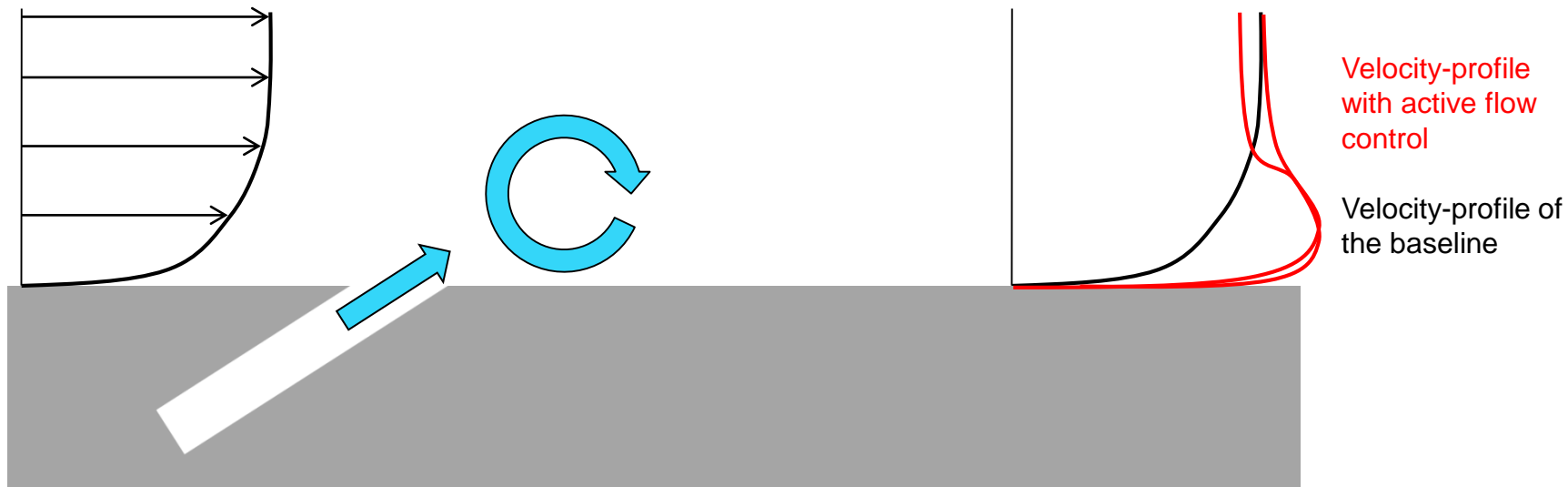
Analysed Configuration

- 7 actuators at the inboard side of the nacelle-wing-junction, total required massflow with pulsed operation: 0.6 to 0.9 kg/s
- Yaw angle: 0°
- Blow angle against the surface 30° : Must be high to reach the free flow to enable the mixing of the boundary layer with the free stream flow



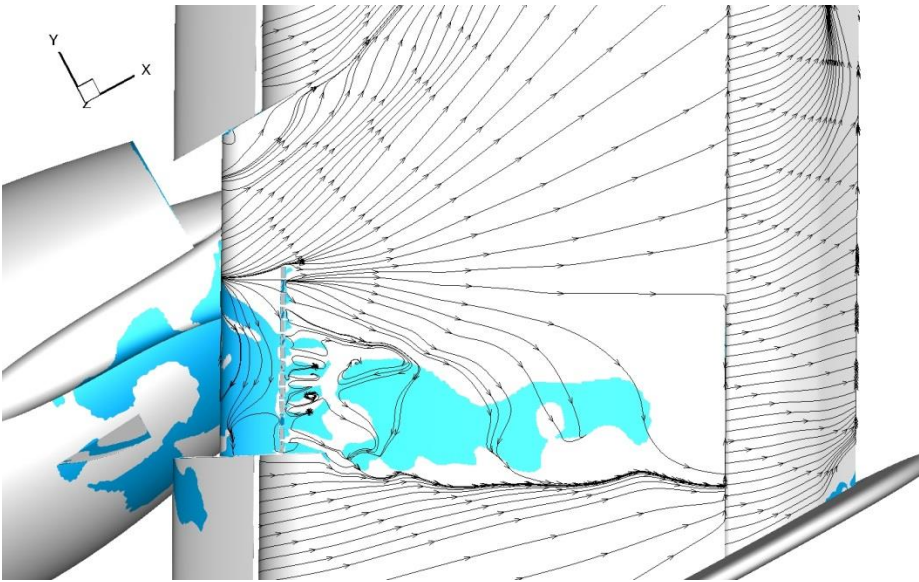
Active Flow Control

- Active flow control → **Active flow separation control** is the **active manipulation of the kinetic energy of the boundary layer**
- Steady blowing directly increases the kinetic energy of the boundary layer
- Pulsed blowing induces vortices which transfer free stream momentum to the boundary layer
- Unsteady blowing can achieve same effect as steady blowing with less air flow

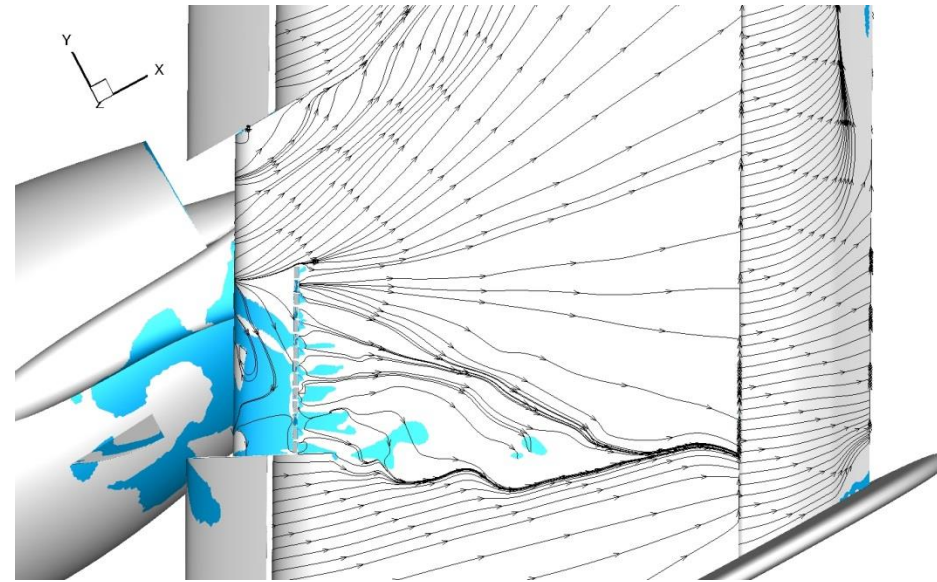


Pulsed Blowing Results: Blowing Velocity

- Exit velocity of 272m/s leads to a suppression of the nacelle-wake-separation
- The introduced impulse with the actuator exit velocity of 200m/s is not sufficient for the suppression of the flow separation



$U_j=200\text{m/s}$ ($dm/dt=0.62\text{kg/s}$), $f=60\text{Hz}$



$U_j=272\text{m/s}$ ($dm/dt=0.84\text{kg/s}$), $f=60\text{Hz}$

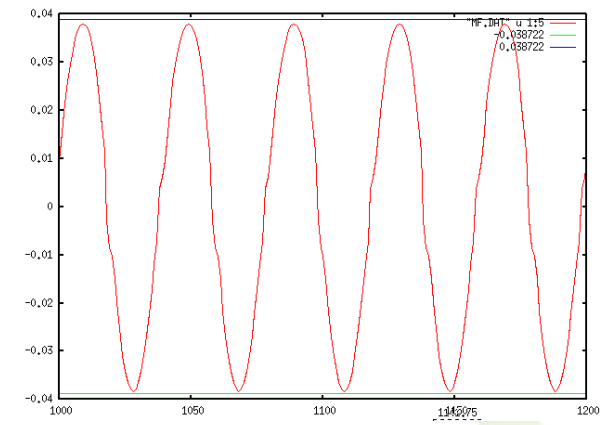
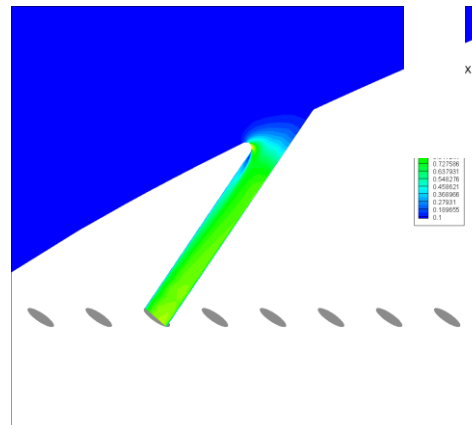


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SYNTHETIC JET ACTUATION

Synthetic jet actuation

- Synthetic jet – zero net mass flux
 - No need for pressure source, electricity driven
 - Suction of air from BL, return with higher energy
- CFD
 - Simulated by mass flow inlet/outlet BC
 - Switching between MF I/O is controlled by step or harmonic function
 - Peak velocity and frequency
 - Sonic velocity at the boundary is limit for the BC → peak velocity



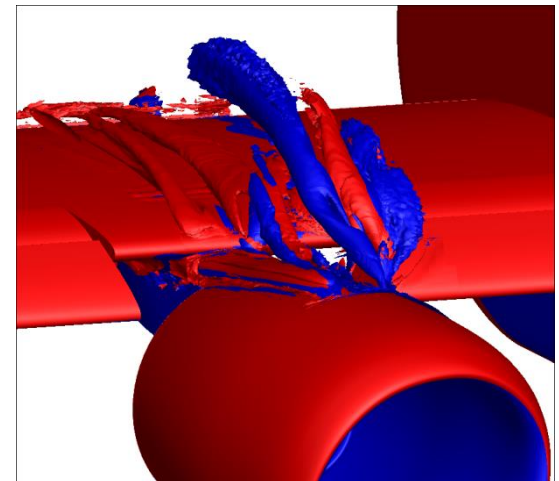
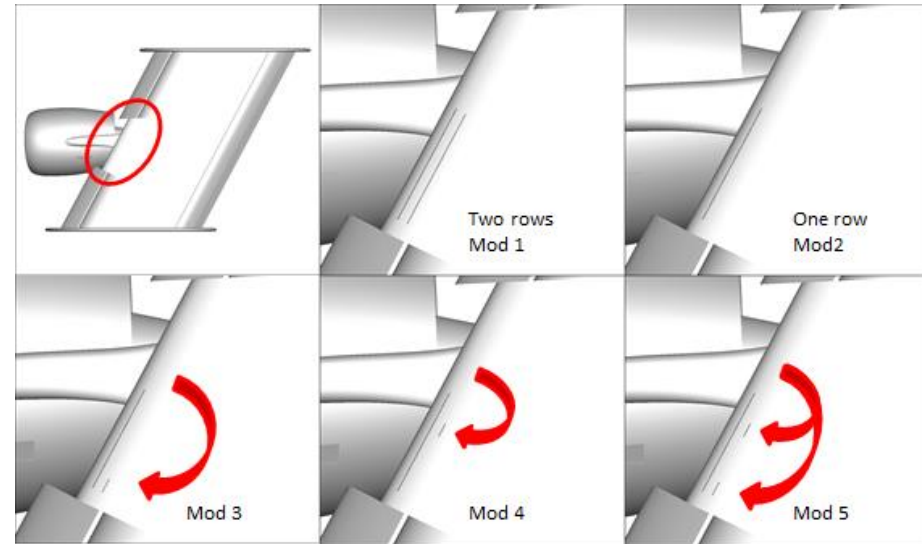
Synthetic jets, set-up

➤ Circular actuator

- Actuator's area 5mm^2
- Pitch angle 30°
- Cavity physically modelled

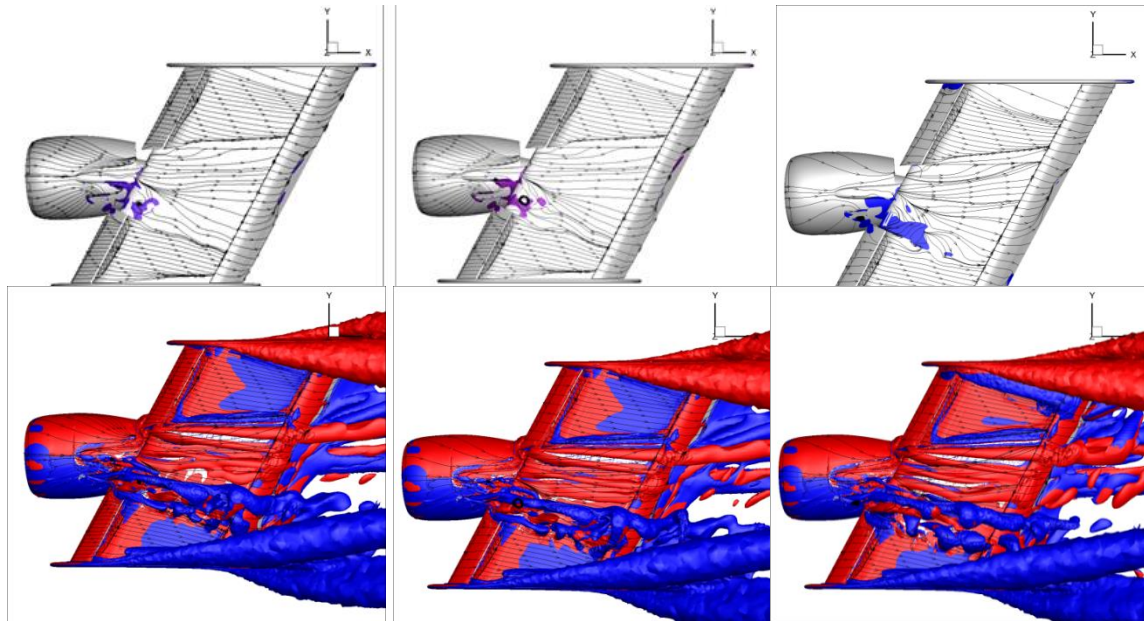
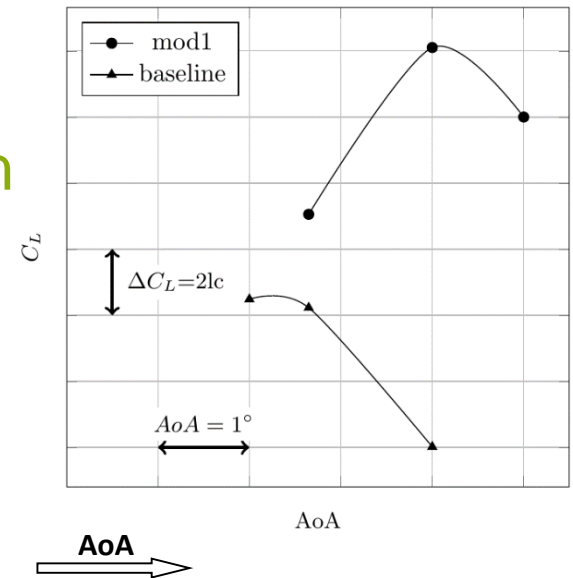
➤ Five configurations

- Actuators in two rows
 - between the inboard slat and pylon nacelle's axis
 - 1st row is located at $0.01\%c$, 85 actuators
 - 2nd row is placed $0.021\%c$, 84 actuators
 - placed in cascade
- One row of actuators
- Three modifications of two rows of actuators
 - Based on structure of vortices



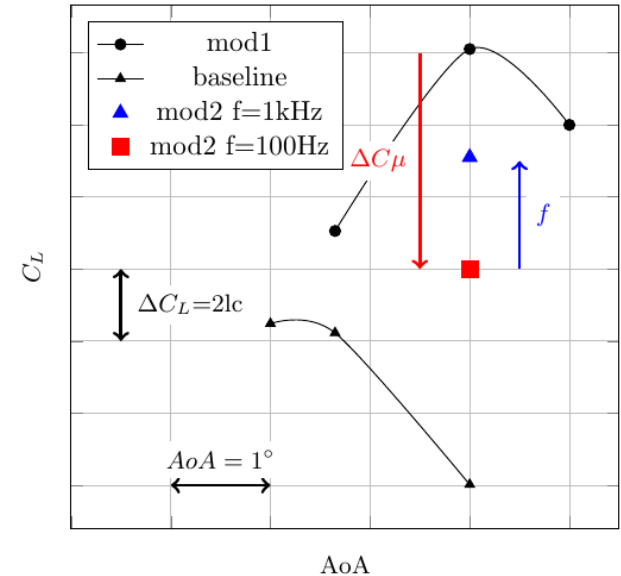
Results – SJA

- Effect of SJA on C_L and flow separation
 - Two rows of actuators
 - Actuation frequency $\rightarrow 100\text{Hz}$
 - Peak velocity $V_j = 150\text{m/s}$
- Stall angle delayed by about 2 deg
- $C_{L,\max}$ improved by about 8 lc

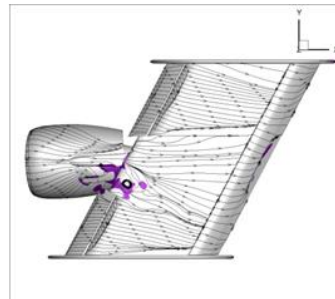


Results – SJA frequency

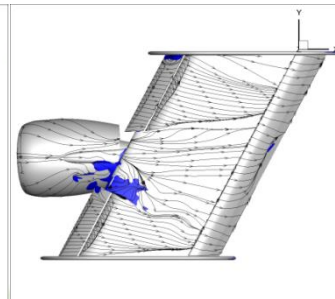
- One AoA ($C_{L,max}$)
 - C_μ and frequency effect
- One row of actuators
 - C_μ to one half compared to two rows
 - Actuation frequency preserved - 100Hz
 - C_L decreased by about $6lc$
- Frequency increased
 - From 100Hz to 1kHz
 - C_L increased by about $3lc$



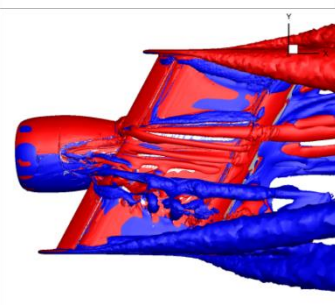
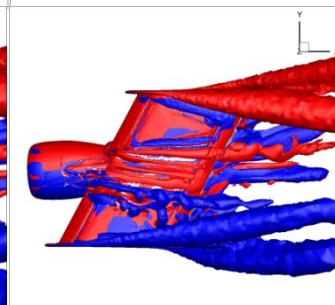
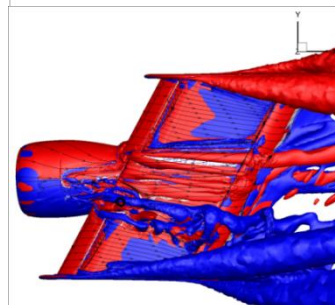
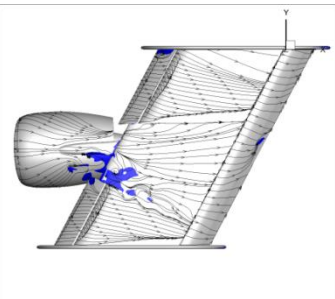
$C_\mu = 0.0252\%$, $f=100Hz$



$C_\mu = 0.0127\%$, $f=100Hz$



$C_\mu = 0.0127\%$, $f=1kHz$



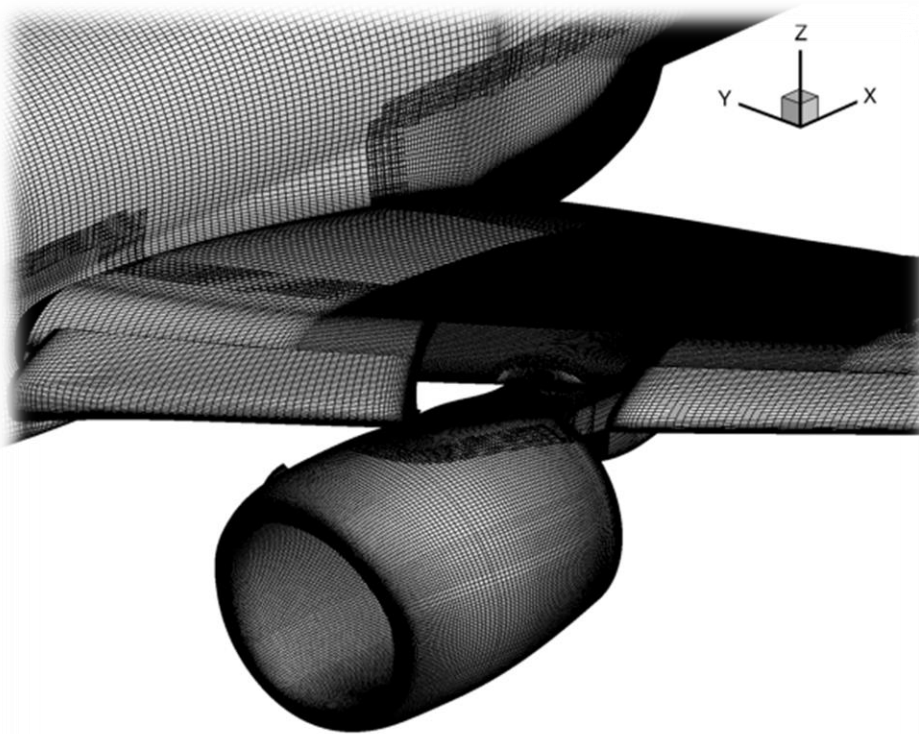


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FULL AIRCRAFT SCALE EVALUATION

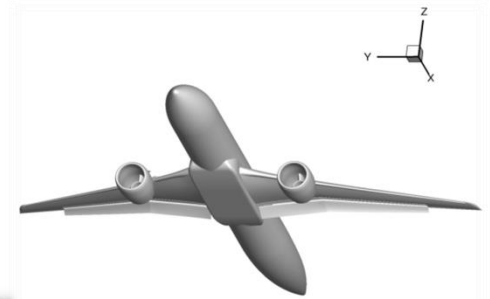
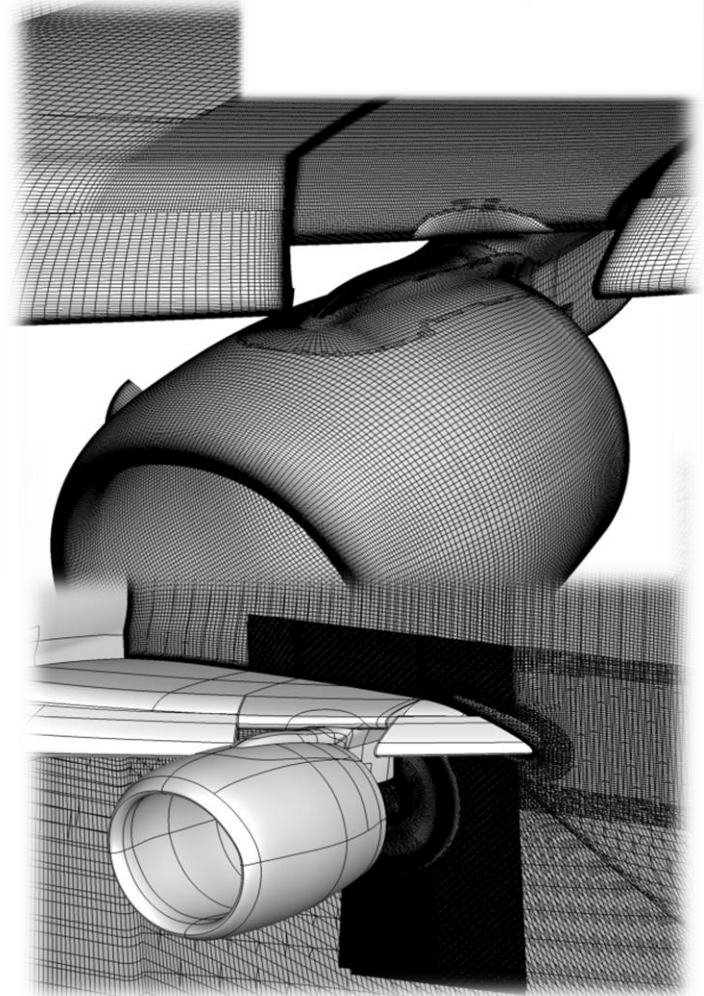
Geometry and grids

- Realistic configuration
 - Structured Overset grid (ca 70 mil cells)



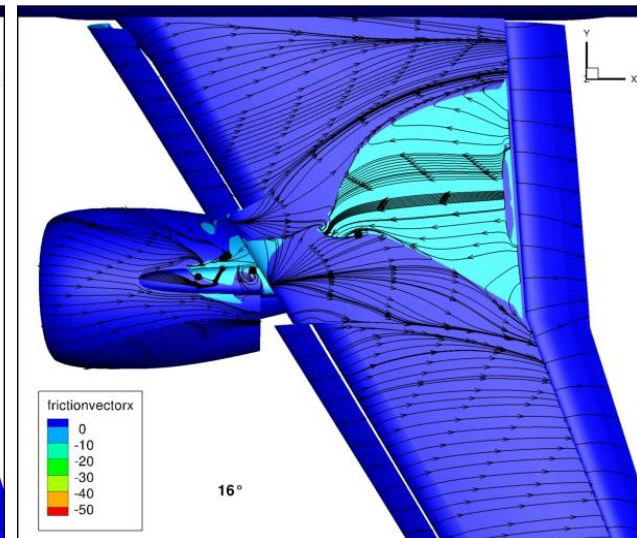
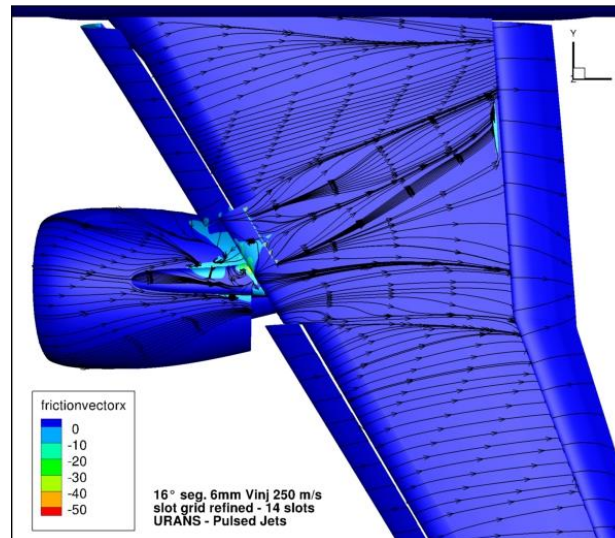
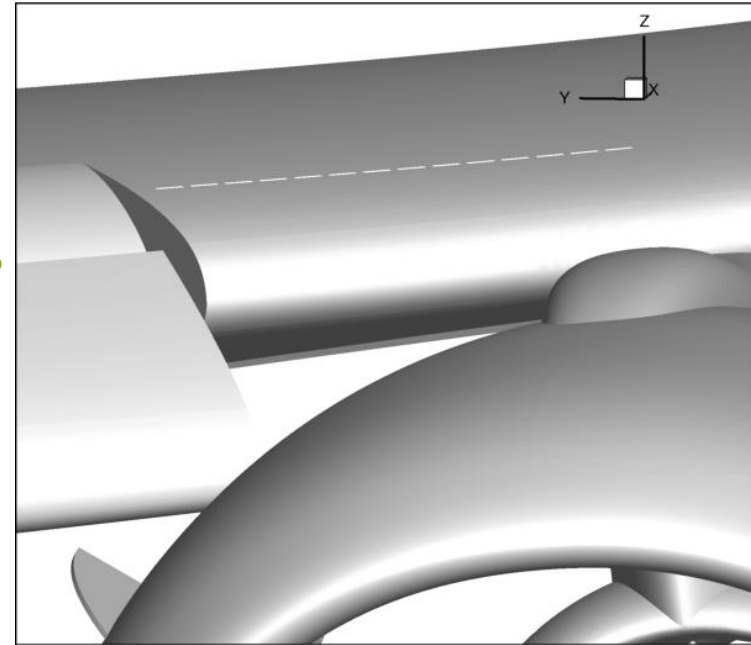
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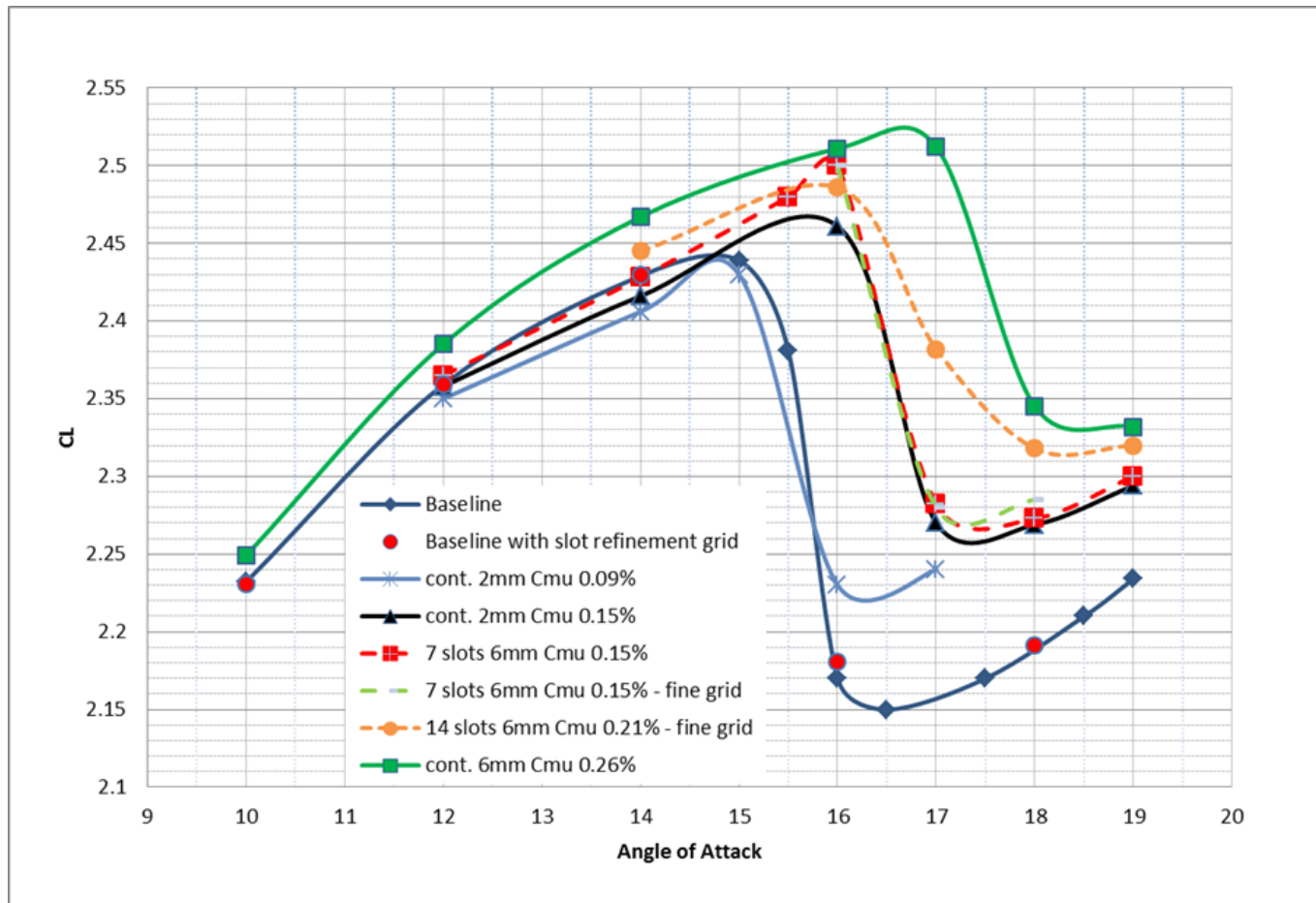
AFC setups

- Steady and pulsed jet blowing slots
 - Variation of slot width (2-6 mm)
 - Jet outlet velocity
 - Influence C_μ
- Pulsed jet blowing
 - $f=60$ Hz, Phase shift
 - Reduced C_μ compared to steady blowing



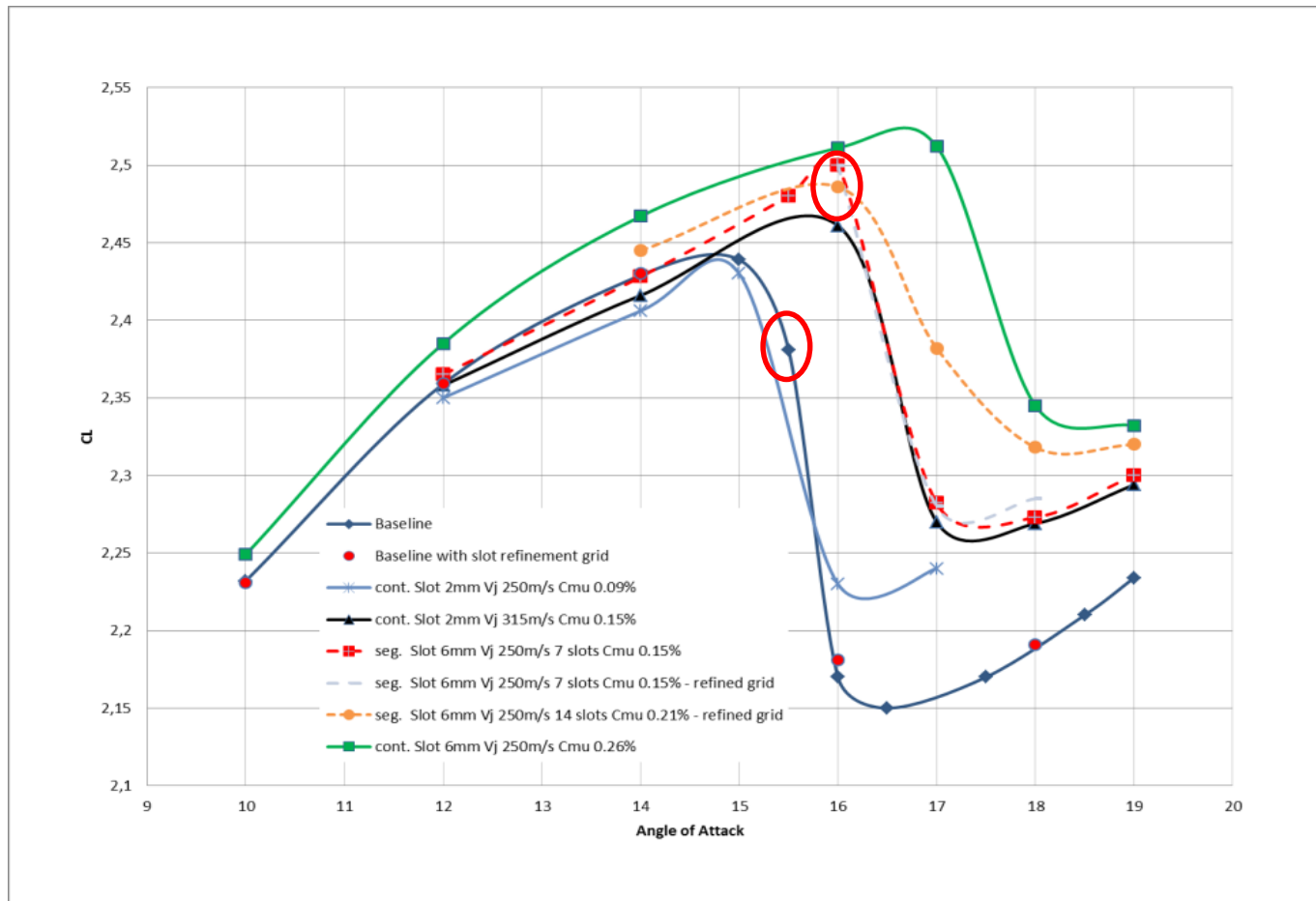
Results of Steady blowing calculations

➤ Effect of C_μ and grid refinement



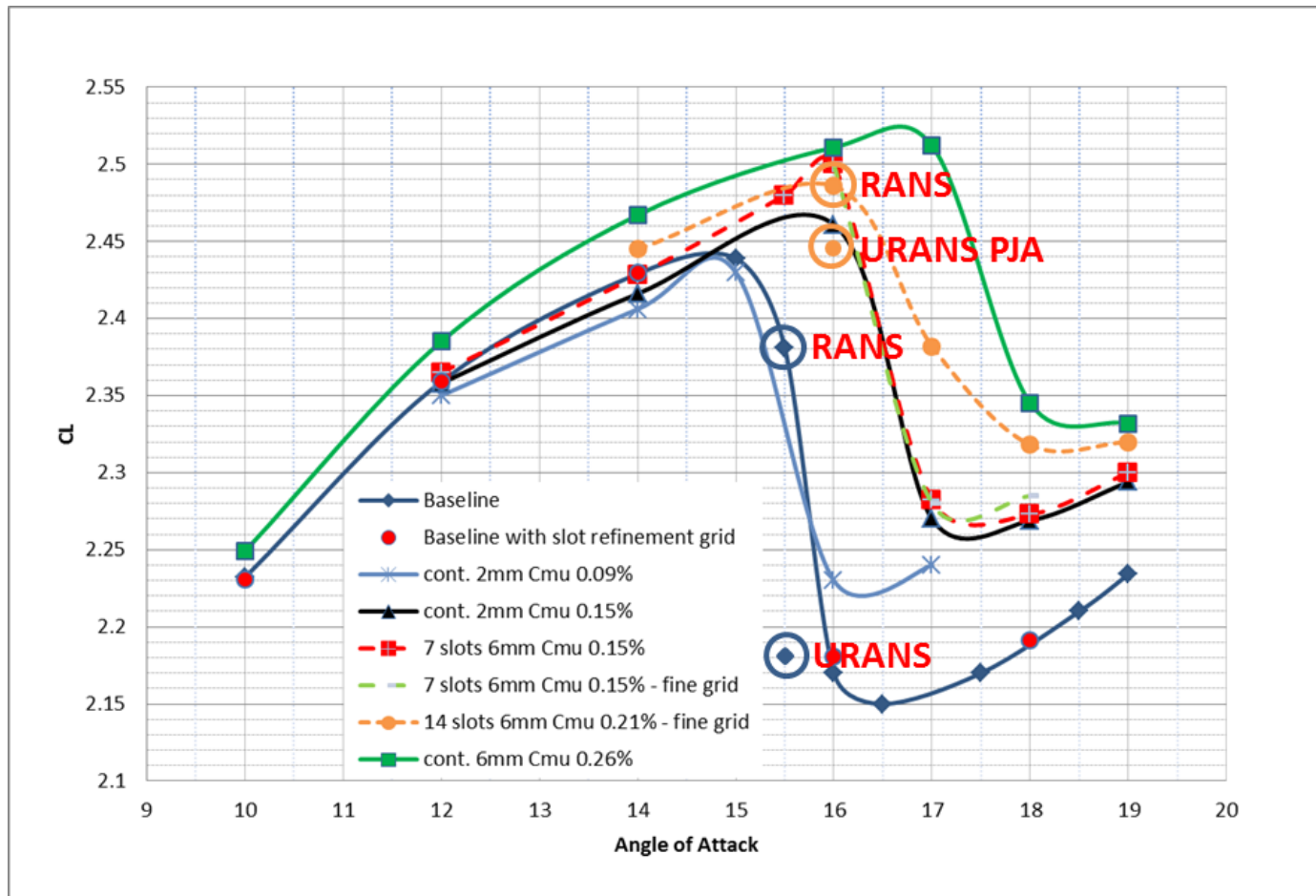
Selected cases for URANS calculations

➤ From RANS with steady blowing to URANS



Results of URANS calculations

- Differences at the stall region – (U)RANS bls., CB / PJ





SUMMARY AND CONCLUSIONS



Summary and Conclusions

➤ CFD tools in theory

- Provide insight into flow behaviour, vortex structure, separation areas
- Parametric studies
- Promising results in terms of separation reduction, $C_{L,max}$ increment

➤ Practical issues

- Lengthy unsteady calculations
- Gap between time scales related to the aircraft and to the AFC
- Results close to stall - needs to be verified by experiment





THANK YOU FOR YOUR ATTENTION!

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